

High gain CPW-fed UWB planar monopole antenna-based compact uniplanar frequency selective surface for microwave imaging

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Running short title: High gain UWB antenna based FSS for MWI

Abstract

In this article, a novel uniplanar ultra-wideband (UWB) stop frequency selective surface (FSS) was miniaturized to maximize the gain of a compact UWB monopole antenna for microwave imaging applications. The single-plane FSS unit cell size was only $0.095\lambda \times 0.095\lambda$ for a lower-operating frequency had been introduced, which was miniaturized by combining a square-loop with a cross-dipole on FR4 substrate. The proposed hexagonal antenna was printed on FR4 substrate with coplanar waveguide feed, which was further backed at 21.6 mm by 3×3 FSS array. The unit cell was modeled with an equivalent circuit, while the measured characteristics of fabricated FSS array and the antenna prototypes were validated with the simulation outcomes. The FSS displayed transmission magnitude below -10 dB and linear reflection phase over the bandwidth of 2.6 to 11.1 GHz. The proposed antenna prototype achieved excellent gain improvement about 3.5 dBi, unidirectional radiation, and bandwidth of 3.8 to 10.6 GHz. Exceptional agreements were observed between the simulation and the measured outcomes. Hence, a new UWB baggage scanner system was developed to assess the short distance imaging of simulated small metallic objects in handbag model. The system based on the proposed antenna displayed a higher-resolution image than the antenna without FSS.

KEYWORDS

CPW, detection, FSS, hexagonal patch, microwave imaging, miniaturizing, ultra-wideband antenna

1 | INTRODUCTION

Variation in the reflection properties of several objects in a conventional handbag appears to be the main motivation of utilizing microwave imaging (MWI) systems to detect hidden metallic object(s) for scanner applications. Non-ionizing radiation, low power level, and low manufacturing cost are some features implemented in the MWI systems, instead of using an X-ray baggage scanner machine.

The ultra-wideband (UWB) imaging system has emerged to be the best candidate due to its broad spectrum that enhances image resolution. UWB antennas are designed with specific traits (broad bandwidth of 3.1–10.6 GHz and high gain) to enhance the construction of images in bag scanner via MWI. As such, a trade-off had been explored between a miniaturized UWB antenna and its low operation frequency. The unidirectional radiation pattern (UDR) antenna is strongly recommended to gain transmitted signals toward the targets, mainly because the scattered signals are observed at an accurate location, which carries the required variation in the features of the detected object(s). Therefore, designing a suitable UWB antenna that presents high performance in meeting all the mentioned requirements is indeed a challenge within the context of MWI application.

UWB patch monopole antennas have been utilized for many MWI applications [1-7]. UDR, high gain, and extensive bandwidth of UWB antenna are required in designing MWI baggage scanner system. The main issue is to obtain UDRs from the UWB planar monopole antenna within the UWB spectrum.

To begin with, a patch monopole antenna [1] was presented with a cavity back to generate UDRs for MWI application. The printed patch monopole antennas [2-5] were presented with metallic reflectors to make the antenna radiate in UDRs. Nonetheless, these reports did not deal with the whole UWB bandwidth, despite the use of high dielectric constant ($\epsilon_r = 9.8$) [4]. Both the cavity-back and metallic reflector were inefficiently generated UDRs within a broad frequency range. As a result, the proposed techniques seemed to minimize the antenna bandwidth with poor radiation efficiency due to out-of-phase reflection [6]. In a recent work, an artificial magnetic conductor (AMC) [8] and an electromagnetic band gap (EBG) [9, 10] were applied as reflectors. Both AMC and EBG suppressed the electromagnetic field of the surface wave at the operating frequency. Both EBG and AMC unit cells were not only large

in size, but also generated a narrow bandwidth and nonlinear phase reflection coefficient [8, 10]. Typically, the uniplanar compact photonic-band gap (UC-PBG) band-pass layers were suspended above the antenna patch as lens or aperture to enhance antenna gain [11-13]. Conversely, the multilayer bandstop frequency selective surfaces (FSSs) were proposed to reflect the back radiation of patch monopole antennas [6, 7] for MWI applications. Although multilayer FSSs can reflect radiation in a wide bandwidth, it can increase both design profile and intricacy.

An FSS operation frequency was operated at $\lambda/2$ of its unit cells electrical length. Demonstrating a finite FSS array size for practical devices by increasing the number of array elements, however, was constricted due to electrical length. Hence, miniaturizing the unit cell size of FSS may exert performances of an infinite array [12].

With that, the primary objective of this study is to design broadband, compact-size, and low-profile FSS array in order to attain UDR and high gain, as well as maintaining the bandwidth of UWB planar monopole antenna. Reflection bandwidth refers to a property of reflecting radiation at a frequency range of 3.1 to 10.6 GHz of UWB with $S_{21} < -10$ dB. Most UWB FSS reflectors in the cutting-edge literature were reviewed and compared. The general impression of these papers referred to the multilayer stop-band FSSs in achieving UWB reflector [6, 7, 14-20]. Nevertheless, the multilayer had cascade spacing between the FSS layers that can increase the overall design size, the manufacturing cost, the intricacy, the nonlinear phase reflection coefficient, and the multipath reflection at the overlapping frequency between two FSS layers.

In general, the UWB stop FSS offers poor phase matching due to the large propagation phase delay variation of the reflected radiations at different frequencies. Literature pertaining to FSS scarcely depicted the phase matching between the direct and the reflected signals, particularly for short spacing between UWB antenna and FSS layers. Hence, literature concerning UWB FSS reflector using FR4 substrate was assessed. Two layers of FSSs were proposed in Refs. [14-17] with a nonlinear reflection coefficient phase, while others looked into linear falling reflection coefficient phase in dual-plane FSSs [6, 18, 19], except in Ref. [20], where the reflection coefficient phase was ignored. Furthermore, the proposed UWB FSS in Ref. [7] had four FSS layers. Although multilayer FSSs in the cutting-edge literature have employed to attain UWB reflectors, the reflected radiations of UWB antenna with FSS have not achieved the complete phase matching.

The multilayer FSSs to date reported to attain UWB bandwidth reflection [6, 7, 14-20]. Nonetheless, only a handful of studies had assessed the linear falling reflection coefficient

phase of FSSs for UDR UWB antenna [6, 18, 19]. In fact, the broad stopband FSS should be relatively large in size due to the low inductive effect and the lower operation bandwidth. The smallest FSS unit cell on FR4 substrate in the literature was reported by Kundu [17] with a size of $0.108\lambda \times 0.108\lambda$ to realize the UWB bandwidth reflector with two-layer FSS, where λ corresponded to the free space wavelength of the lower operation frequency with a transmission coefficient lower than -10 dB. To the best of the author's knowledge, a uniplanar compact-size low-cost FSS that led to linear decreasing reflection coefficient phase of UWB stop response has not been reported in the literature.

In this article, a uniplanar UWB FSS was miniaturized to improve the UWB antenna gain for MWI application. The rest of this paper was organized as follows. In Section 2, both copper square-ring and cross-dipole were combined on the top side of FR4 substrate to serve as a broad bandwidth reflector. This compact unit cell gave a reflection performance within the 2.6 to 11.1 GHz range and generated a linear decline of the reflection phase over the entire UWB spectrum. Thus, this study investigated the theoretical operation mechanism and the equivalent circuit of the proposed unit cell. In Section 3, 3×3 FSS array was formed with UWB patch monopole antenna, successfully generated high-gain and UDR due to the phase matching. In Section 4, the FSS array and the proposed UWB antenna with FSS prototypes were measured and validated with the simulated results from CST Microwave Studio for empirical characterization. In Section 5, a new MWI baggage detection approach was developed based on the proposed UDR monopole antenna. Finally, a conclusion was addressed in Section 6.

2 | THE PROPOSED FSS DESIGN

2.1 | FSS design and its operation

Figure 1a illustrates a 3D view of the FSS array. The metal layer was a combination of a square-ring and a cross-dipole in multiple periodic cells of the array. The symmetrical spacing (s) between the metal unit cells observed a capacitive act (C_c) for each neighbor cell to achieve reflection at a lower frequency with small spacing. The FSS array had a substrate thickness (T_{fsb}). The UWB stop FSS unit cell geometry, along with several related parameters, is displayed via 2D top view in Figure 1b. The physical dimensions of D_x and D_y of the unit cell are presented in xy plane.

The following process was performed to attain the broad bandwidth of FSS unit cell. First, the copper square-ring was loaded on top of the FR4 substrate. The square-ring reflected radiation at lower frequency with the entire electrical length of $\lambda/3$ [21]. Second, the width of

square-ring (g) was increased to obtain a low inductance (L_s) value while the spacing (s) was decreased to attain a high capacitance (C_c) value. Thus, the bandwidth of the unit cell was enhanced. The empty area in the center of the square-ring had small capacitance (C_s) that allowed high frequencies to pass. Third, on the same layer, a copper cross-dipole was printed in the center of the substrate to reflect the radiation at high frequency with dipole electrical length of $\lambda/2$. Fourth, the cross-dipole length was increased and connected to the square-ring. The cross-dipole decreased the free area in the center of the square-ring, hence generating high parallel inductance (L_c) and higher series capacitors (C_s) values due to the small cross width (W_{fc}) and the four triangular free areas, respectively. As a result, the FSS bandwidth was substantially enhanced. The complementary structure of the proposed FSS unit cell attained reflection radiation of both lower and higher frequencies over the UWB spectrum. The aforementioned process pointed toward miniaturized unit cell size and enhancement of the bandwidth.

The bottom layer of the unit cell was metal-free. Hence, a small static capacitance (C_o) of the FSS layer was demonstrated. Assuming that the array structure had a size of period unit cells, the capacitor, C_c , was observed for each cell with the neighboring cells. The effective length of FSS unit cell (L_{fss}) in mm was determined by the following:

$$L_{fss} = Lfs - g + \frac{Lfc - Wfc}{2} \approx \frac{c}{2f_o \sqrt{(\epsilon_r + 1)/2}} \quad (1)$$

Where c stands for velocity of light in free space (3×10^8 m/s), f_o is resonating frequency and ϵ_r refers to relative permittivity of the dielectric used.

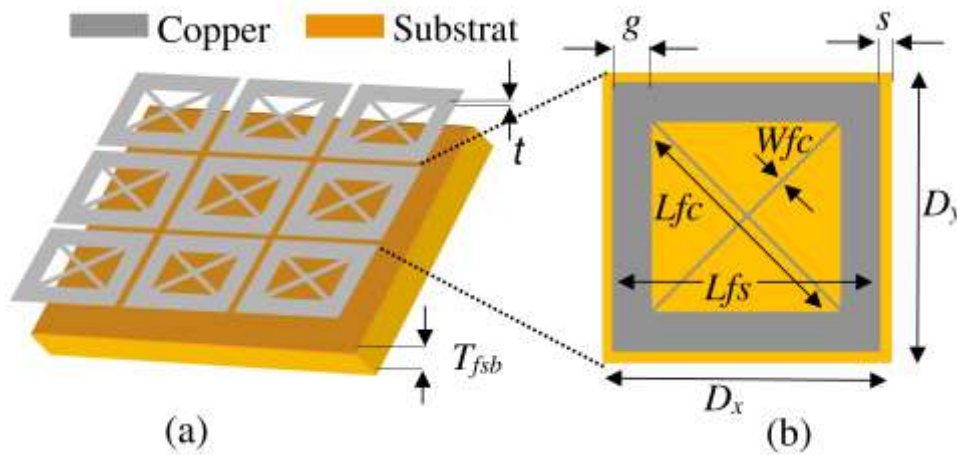


FIGURE 1 Geometry of (a) FSS array, and (b) FSS unit cell

2.2 | FSS equivalent circuit model

To further comprehend the operation of this FSS unit cell structure, the equivalent circuit model (ECM) is as portrayed in Figure 2. Generally, the ECM of the conventional square-ring loop FSS unit cell (band-stop filter) can be modeled as series-shunt inductance (L) and capacitance (C) resonator. The size of the metallic loop was modeled into the FSS inductance, while the spacing on both sides of the metallic element generated the capacitance model due to the neighboring cells [22]. The LC values of the FSS cell were calculated based on size, structure, and substrate materials.

Basically, the self inductance of a metallic stripe was obtained by using the calculation used in Ref. [23] for metallic length and width. The capacitance between any parallel metallic structures was obtained based on the relation between the metallic facing area and the spacing. Both the permittivity in free space ($\epsilon_o \approx 8.854 \times 10^{-12}$ F/m) and the relative permittivity (ϵ_r) of the material between the parallel metallic plates were considered. The substrate of unit cell reflected a sandwich model, as presented by a short length of line transmission (ht) in Figure 2. This transmission line referred to: impedance $Z_T = Z_o/\sqrt{\epsilon_r}$. Where $Z_o = 377 \Omega$ is known as wave impedance in free space, while ϵ_r refers to the relative permittivity of the dielectric substrate. As the substrate was located behind the metallic plane of the model, the impedance (Z_T) was linked in series between the static capacitance, C_o , of the FSS and Z_o .

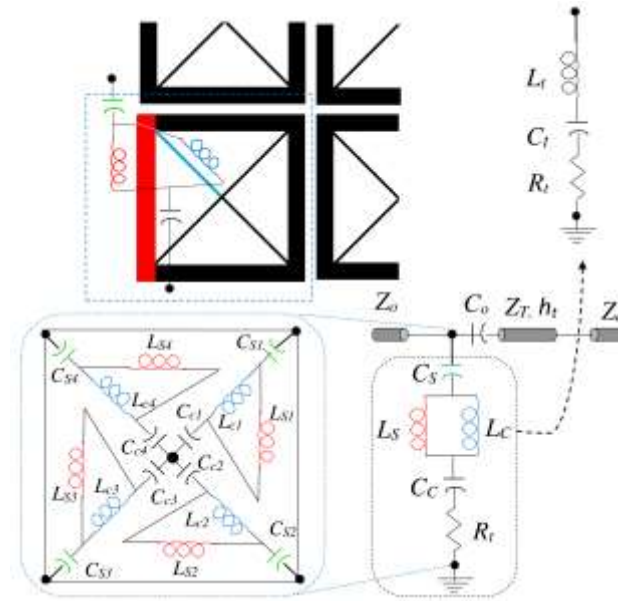


FIGURE 2 FSS equivalent circuit model

This study proposed the connection between the square-ring loop FSS and cross-dipole FSS on a single-layer unit cell without any ground plane. The explored capacitance, C_S , between the adjacent FSS cells can be disregarded to simplify the calculation of the whole model. However, in this design, C_S was weighed in due to its effect on reflection bandwidth. In order to increase the reflection bandwidth with slightly altering the center frequency, the spacing between the metal of the neighboring unit cells ($2 \times s$) was reduced. This capacitance was derived based on the proposed unit cell parameters, as given in Equation (2):

$$C_S \approx \epsilon_o \epsilon_r \frac{L_{fs} \times t}{2s} \quad (2)$$

The square-ring generated a broad reflection bandwidth. Therefore, inductive L_S was derived based on the square-ring parameters, as presented in Equation (3):

$$L_S \approx 2L_{fs} \times \ln \left(\frac{2L_{fs}}{g+t} + 0.5 + \frac{g+t}{3L_{fs}} \right) \quad (3)$$

The additional self inductance, L_C , of the cross metal was connected parallel to L_S , which shifted the upper edge of the reflection bandwidth to a higher frequency. The cross metal divided the inner area into four small parts. The spacing between the cross and the square was represented by series capacitance, C_C . Based on the unit cell parameters, L_C and C_C of the analyzed ECM were determined via Equations (4) and (5), respectively:

$$L_C \approx 2L_{fc} \times \ln \left(\frac{2L_{fc}}{W_{fc}+t} + 0.5 + \frac{W_{fc}+t}{3L_{fc}} \right) \quad (4)$$

$$C_C \approx \epsilon_o \epsilon_r \frac{(L_{fs} - 2g) \times t}{(L_{fs} - 2g) / 2} \quad (5)$$

To simplify the proposed ECM, the total inductor, L_t , was derived from the parallel inductors, L_S and L_C . The total capacitor, C_t , was incorporated from the series capacitors, C_S and C_C , to obtain resonance frequency and broad bandwidth, while the FSS static capacitor, C_o , was controlled to attain the bandstop filter bandwidth. The total resistance, R_t , of the unit cell was connected in series to both L_t and C_t , which managed the transmission magnitude in dB due to substrate losses and cell resistance. The simplified RLC circuit gave the total impedance, Z_{fss} , of the proposed unit cell, as given in Equation (6):

$$Z_{fss} = R_t + j \frac{\omega^2 L_t C_t - 1}{\omega C_t} \quad (6)$$

After simplifying Equation (6), the ECM resonance frequency was obtained using Equation (7) as follows:

$$f_r = \frac{1}{2\pi\sqrt{L_t C_t}} = \left(\frac{1}{2\pi}\right) \sqrt{\frac{(L_s + L_c) \times (C_s + C_c)}{L_s L_c C_s C_c}} \quad (7)$$

The insertion loss of *RLC* circuit exhibited a broad bandstop characteristic after calculating the bandwidth, *BW*, using Equation (8), as reflected in the following:

$$BW \approx R_t / L_t C_o \quad (8)$$

2.3 | FSS simulation and results

The unit cell was printed on a square FR4 substrate with dielectric constant (ϵ_r) of 4.3, loss tangent ($\tan\delta$) of 0.025, thickness T_{fsb} of 1.6 mm, and area $D_y \times D_x$ of 11×11 mm². The proposed copper structure had a height (t) of 0.035 mm printed on the top layer of the substrate. The compact uniplanar unit cell was designed without any ground plane for the bottom layer of the substrate. The copper square-ring had a side length, L_{fs} , of 10.8 mm; a width, g , of 1.6 mm; and spacing substrate edge, s , of 0.1 mm. The cross-dipole parameters were as follows: the length of arms, $L_{fc} = 10.6$ mm, and the width of arms, $W_{cf} = 0.3$ mm, as illustrated in Figure 1b.

The electromagnetic characteristics of the unit cell were obtained from CST Microwave Studio, as shown in Figure 3a. Both the simulated transmission and the reflection coefficients are portrayed in Figure 3b by using normal incidence. As a result, the tested FSS unit cell displayed broad bandstop performance. The transmission coefficient exhibited a magnitude below -10 dB for the range between 2.6 and 11.1 GHz, which was realized with a unit cell size of $0.095\lambda \times 0.095\lambda$. The transmission coefficient achieved center stop frequency at 6.5 GHz by simulating the proposed unit cell.

Figure 3b displays the reflection coefficient phase ($S_{11} \angle_{FSS}$) in degree of the FSS. The $S_{11} \angle_{FSS}$ linearly decreased with increment in the frequency over the whole UWB spectrum. Typically, the reflected radiation delay of 2π , which was compatible with the direct antenna radiation phase, was realized by generating a stable $S_{11} \angle_{FSS}$ curve slope. This condition was satisfied at a constant distance, D_z , of $\leq \lambda_o/4$ between wideband antenna and FSS array, where λ_o refers to a wavelength of zero reflection phase shift.

The S-parameters of the proposed ECM was computed by using the schematic circuit of CST software to validate both the simulated design and the proposed circuit. Both calculation and optimization processes were performed to determine the *RLC* values that met similar resonance frequency and bandwidth of the stop band. The ECM parameters had optimum values, as follows: $L_s = 2.8$ nH, $L_c = 8.6$ nH, $C_s = 8.1$ pF, $C_c = 0.295$ pF, $C_o = 0.085$ pF, and

$R_t = 1.2 \Omega$. The schematic of CST software portrayed a significant agreement between the ECM and the unit cell outcomes, as presented in Figure 3b.

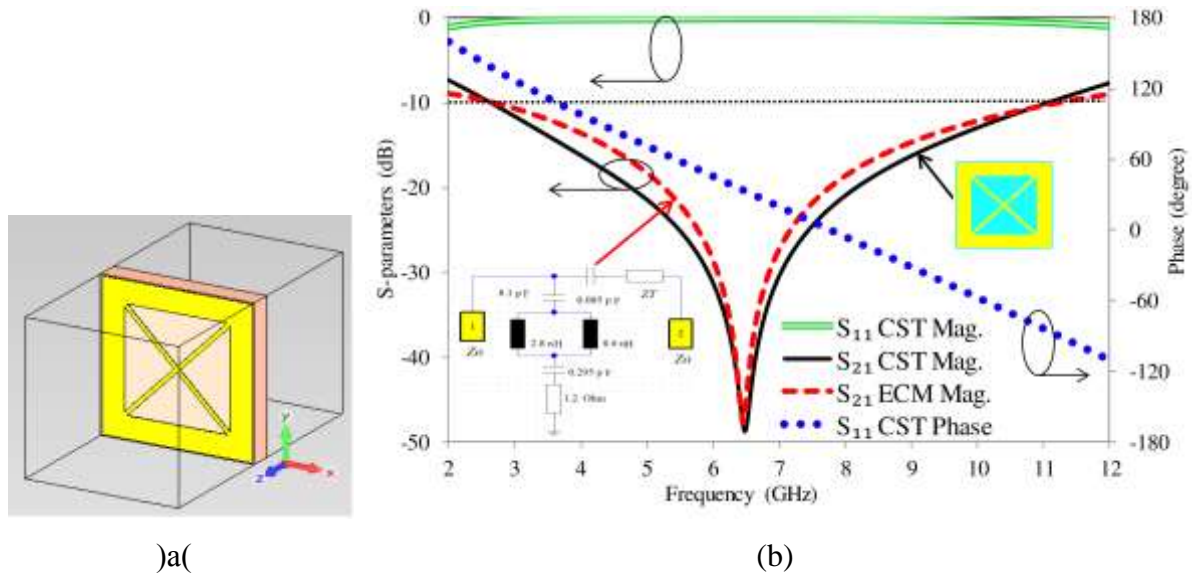


FIGURE 3 (a) Diagram of the simulation model (b) simulated transmission and reflection coefficients

The simulated outputs highlighted two main points. The first point is that the unit cell parameters were tuned to produce broad reflection bandwidth. The second point is that the center resonance frequency of the unit cell was assessed. Based on Equation (7), reducing the total unit cell size can shift the center reflection to a higher frequency. As such, a large unit cell size was required to realize reflection at low resonance frequency, which appeared to be a challenge amongst researchers. The use of high dielectric constant substrate can address this issue, as given in Equation(1). Nonetheless, this study had been limited to low-cost manufacturing using FR4 substrate. The $S_{11} \angle_{FSS}$ displayed a linear decreasing slope ($\Delta\text{Ph}/\Delta F$) of $-27^\circ/\text{GHz}$. The antenna gain can significantly improve for the UWB spectrum due to the obtained linear $S_{11} \angle_{FSS}$. The negative slope of $S_{11} \angle_{FSS}$ approximately equalized the positive slope of path delay phase for the broad bandwidth.

The current distribution on the metallic surface was simulated at varied frequencies to determine the reflection mechanism of the proposed FSS structure. A high current flow was observed on both the square and cross shape at a low frequency of 4.0 GHz, as illustrated in Figure 4, while current highly flowed on the cross-shape at a high frequency of 8.0 GHz due to the electrical length.

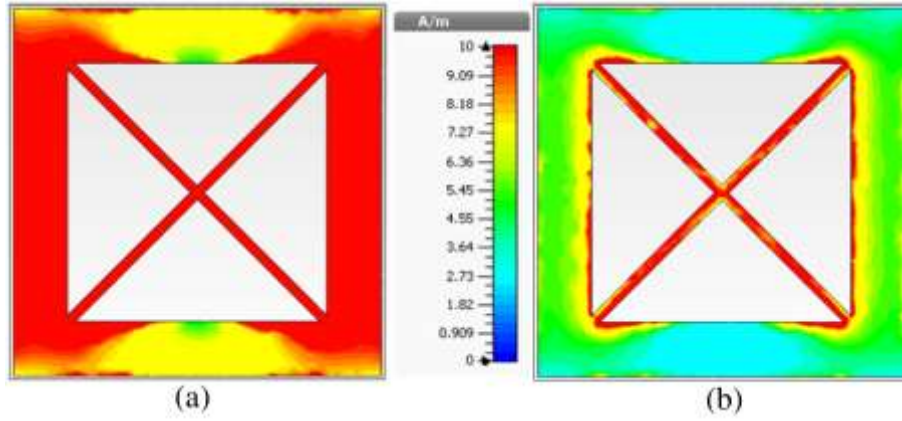


FIGURE 4 Current distribution on FSS unit cell at (a) 4.0 GHz, and (b) 8.0 GHz

3 | FORMING UWB MONOPOLE ANTENNA WITH FSS REFLECTOR

The FSS design delineated in Section 2 was applied to improve the performance of monopole antenna at UWB spectrum. The geometry and the characteristics proposed hexagonal UWB monopole antenna, as comprehensively discussed in Ref. [24]. Figure 5a portrays the parameters of the uniplanar hexagonal patch monopole antenna with coplanar waveguide (CPW) feed (Antenna #1). The antenna printed on FR4 substrate shared similar thickness (H) and properties of the FSS substrate. To design the antenna with CPW-fed, two copper ground planes were adjusted on the sides of the feed line by a distance of ($Scpw$). The CPW-fed parameters were analyzed and optimized to achieve 50Ω impedance of the feed line. The hexagonal patch was modified to enhance the antenna bandwidth. The hexagonal patch parameters were as follows: a short side (S_1), long side (S_2), radius (R), and angle (a°), as depicted in Figure 5a. The values of UWB antenna parameters are tabulated in Table 1. Lower band-edge (f_L) of the proposed antenna was calculated by equating area of the planar antenna and an equivalent cylindrical monopole antenna, as given in Equation(10) [25]. The equivalent cylindrical parameters of the proposed hexagonal patch with unequal angles and sides length were derived, as given in Equation (9):

$$R = \frac{S_1}{[2 \times \sin(a)]}, \quad L = 2 \times R, \quad \text{and} \quad r = \frac{[2 \times R \times \sin(a) \times \cos^3(a)]}{\pi} \quad (9)$$

$$f_L = \frac{c}{\lambda} = \frac{7.2}{[(L + r + p) \times k]} \text{ GHz} \quad (10)$$

where L is the height of the planar monopole antenna in cm, r (cm) refers to the effective radius of equivalent cylindrical monopole antenna, p represents the probe length, and $k = 1.15$

reflects the constant for FR4 substrate. The hexagonal patch monopole antenna was selected to operate in front of the FSS array reflector.

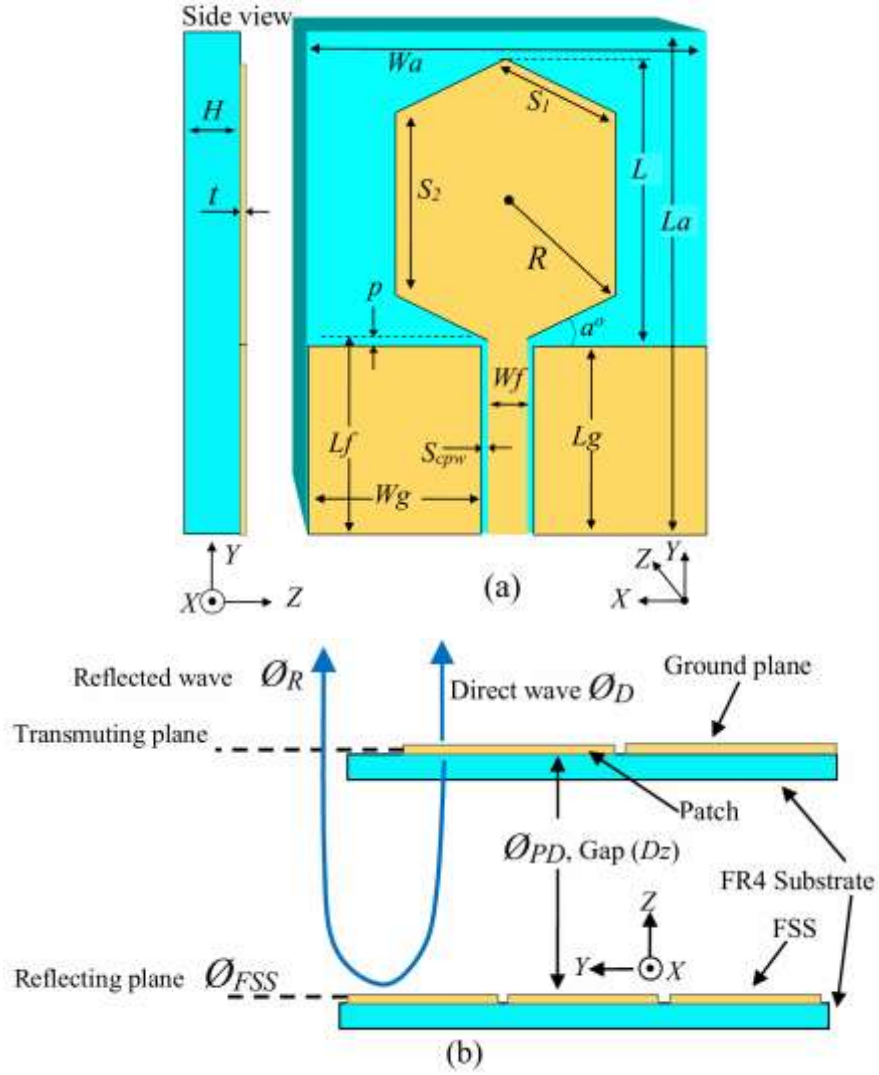


FIGURE 5 (a) Antenna #1 parameters on 3D and side views, and (b) side view of Antenna #2

TABLE 1. The parameters of the proposed hexagonal patch monopole antenna

Parameter	Value (mm)	Parameter	Value (mm)
S_1	8.5	$Scpw$	0.27
S_2	11	Wg	14.3
t	0.035	Lg	11.1
Wf	2.5	Wa	31.9
Lf	11.4	La	30
p	0.4	H	1.6
a°	24°	R	10.45

In this study, a numerical method was employed to determine the distance (D_z) between the antenna and the proposed FSS reflector. Based on the antenna size, 3×3 unit cells were organized in a single-layer rectangular array FSS. Figure 5b illustrates Antenna #1 that was formed with the FSS array printed on the FR4 substrate with D_z spacing. The distance, D_z , was calculated carefully to enhance the antenna gain by reflecting the back radiation. Therefore, a parametric study of Antenna# 2 with FSS array at different spacing D_z can illustrate the performance enhancement.

The simulated reflection coefficients of Antenna #2 were studied at the different distances of D_z as shown in Figure 6a. From the simulation study, both gain and bandwidth of Antenna #2 were investigated by varying the spacing D_z between the FSS array and the antenna. Figure 6b portrays the variation of D_z in x-axis from 14.6 to 29.6 mm. Lower frequency (Fl) and higher frequency (Fh) of the antenna resonance bandwidth ($S_{11} < -10$ dB), peak gain at Fl , and peak gain at Fh of the antenna were represented in y-axis. The resonance bandwidth ($Fl = 3.2$ GHz to $Fh = 12.5$ GHz) was significantly improve at $D_z = 21.6$ mm, but decreased at other D_z values. Moreover, the maximum peak gain of Fh was realized at 8 dBi and 21.6 mm spacing, while the peak gain of Fl smoothly dropped from 7.0 to 3.4 dBi by increasing the D_z from 14.6 to 29.6 mm. A trade-off was noted between the peak gain at Fl and the peak gain at Fh after varying the spacing, D_z . This was attributable to the phase matching between the front and the reflected signals at a particular frequency. The antenna gain can be improved when the reflected signals have a phase of $(n \times 2\pi)$ to the front signals.

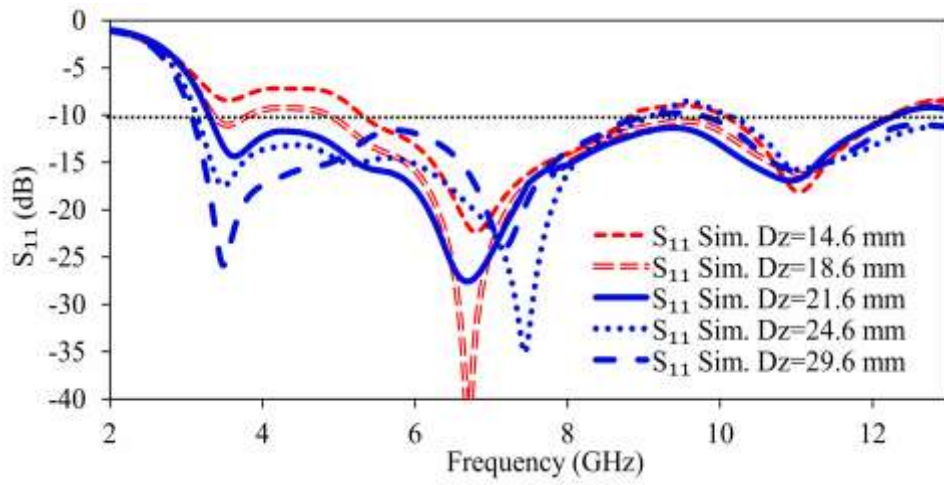
The phase shift of Antenna #2 was further analyzed at $D_z = 21.6$ mm due to the maximum operation bandwidth and optimum gain enhancement. The total phase shift of the reflected signal was calculated by considering the path delay phase (ϕ_{PD}) and the FSS phase (ϕ_{FSS}), as given in Equation (11). ϕ_{PD} mainly relied on distance, D_z , and a particular frequency calculated using Equation (12). The normal incidence was considered, in which the incident wave was perpendicular to the FSS layer (incident angle, $\theta = 0^\circ$) and air gap, $\epsilon_r = 1$, the numerical calculation of $D_z = 21.6$ mm led to $\phi_{PD} = 2\pi$ at 6 GHz (see Figure 6c). The proposed FSS gave a linear falling of ϕ_{FSS} , which approximately equalized the linear increase of ϕ_{PD} over the UWB spectrum. The simulated reflection coefficient phase ($S_{11}\phi$) unwrapped of both the proposed FSS unit cells and the UWB antenna were imported into the workspace. The UWB back radiation was successfully reflected with FSS array.

$$\phi_R(f) = 2\phi_{T, \text{Ant}}(f) - \phi_{PD}(f) - \phi_{FSS}(f) = \phi_D(f) + 2n\pi \quad (11)$$

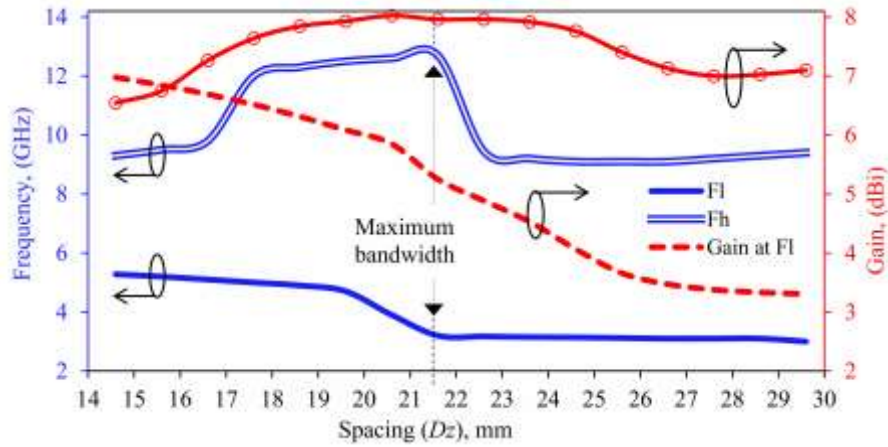
where $n = \pm 1, \pm 2, \pm 3, \dots$

$$\phi_{PD}(f) = 2\beta \times Dz \times \sqrt{\epsilon_r - \sin^2(\theta)}, \quad \beta = \frac{2\pi}{\lambda} \quad (12)$$

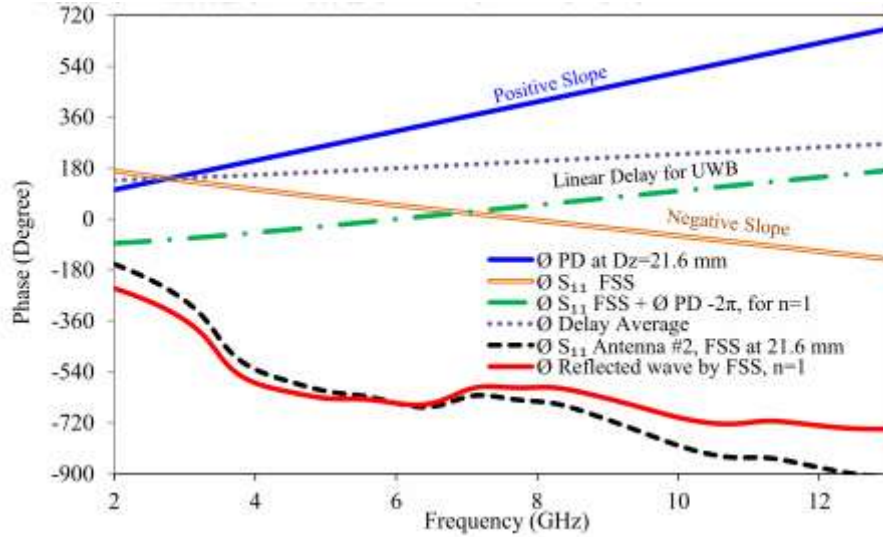
where ϕ_R is the phase of reflected wave, ϕ_D is the phase of direct wave (see Figure 5b), ϕ_T is the transmission phase of the antenna, f is the operating frequency, λ is the wavelength, β is the propagation constant of free space, θ is the incident angle, ϵ_r is the dielectric constant of spacing (air), and Dz is the spacing distance.



(a)



(b)



(c)

FIGURE 6 Simulated variation of Antenna #2 reflection coefficients in (a), study of antenna bandwidth and gain in (b) at the different distances of Dz , and (c) the transmitted and reflected (reflected wave) unwrap Antenna #2 phases

Based on the mathematical calculation in Equations (11) and (12), the reflected signal obtained a phase of the moving path ϕ_{PD} of $(2 \times \beta \times Dz)$ sum with ϕ_{FSS} . The summation results of the Equation (11) parameters are portrayed in Figure 6c. The sum phase vector had a delay of $(1 \times 2\pi)$ due to the moving path ϕ_{PD} . The final outcomes are presented in Figure 6c by setting $n = 1$ and $Dz = 21.6$ mm, which displayed exceptional agreement between the antenna phase shift and the reflected signal phase. In brief, the proposed FSS array demonstrated $1 \times 2\pi$ phase shift between the direct and the reflected signals at 6 GHz when $Dz = 21.6$ mm.

The reflected signal phase was compatible with the direct signal phase for the entire UWB spectrum. Thus, the antenna gain and the bandwidth were improved by simulating the complementary design at $Dz = 21.6$ mm. Next, Figure 7 illustrates the simulated antenna gain and return loss (magnitude) of both with and without FSS array. The antenna gain sharply improved (from 4.8 to 7.8 dBi) for all UWB spectra with the proposed FSS array. The antenna gain could be further enhanced by increasing the number of cells for the FSS array.

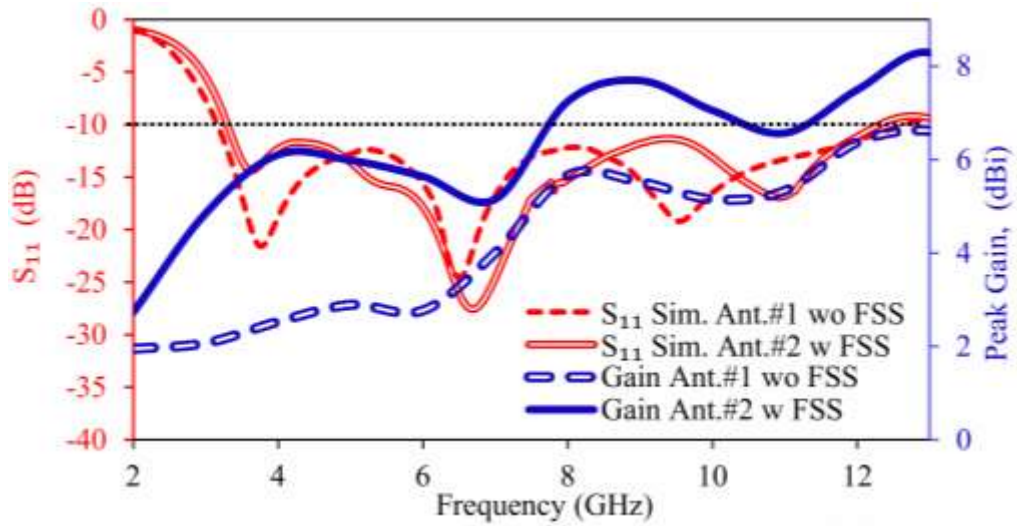


FIGURE 7 Validation of simulation for Antennas #1 and #2 return loss and peak gain

4 PROTOTYPES FABRICATION AND MEASUREMENT RESULTS

4.1 | Experimental results of FSS array

For further validation, a prototype of the single-layer FSS array was fabricated on FR4 substrate. Figure 8a shows the FSS array prototype with 54×36 elements, whereas Figure 8b presents the zoom view of the FSS unit cells prototype. Two opposite horn-antennas were applied to measure the transmission coefficients of the fabricated prototype. The bi-static free space measurement was performed by connecting two horn-antennas to B&S ZVB14 Vector Network Analyzer [26]. Initially, the calibration was carried out for the fixed antennas above absorber with a spacing of 100 cm between them. After that, the measured transmission coefficient was normalized without incorporating the FSS array. Next, the FSS array was placed between the antennas, as shown in Figure 8c. Subsequently, two adjacent horns were placed at a distance of 50 cm from a copper plate, which has a size as same as the FSS array to calibrate a reference S_{11} . Then, the reflection coefficient was normalized by incorporating the copper plate. The reflection coefficient was measured by placing the FSS array, instead of the copper plate, as shown in Figure 8d. The normal incidence was weighed in to determine the transmission coefficient of the transverse electric wave. The measured S_{21} and S_{11} magnitude were recorded from the network analyzer.

Both the simulated and measured S-parameters of fabricated FSS prototype, as shown in Figure 8e, displayed good agreement between the measurement and simulation outcomes. Interestingly, the measured stop bandwidth ranged between 3.2 and 11.3 GHz, while the minimum transmission magnitude was -41 dB at 7.0 GHz. The ripples of the results were

polished by using the smooth average option, which were generated from coaxial cables and connections losses. The FSS prototype was printed on the lossy substrate by using the conventional process. The center frequency of the measured transmission coefficients was shifted slightly to a higher frequency due to fabrication tolerance, in comparison to simulation outcomes.

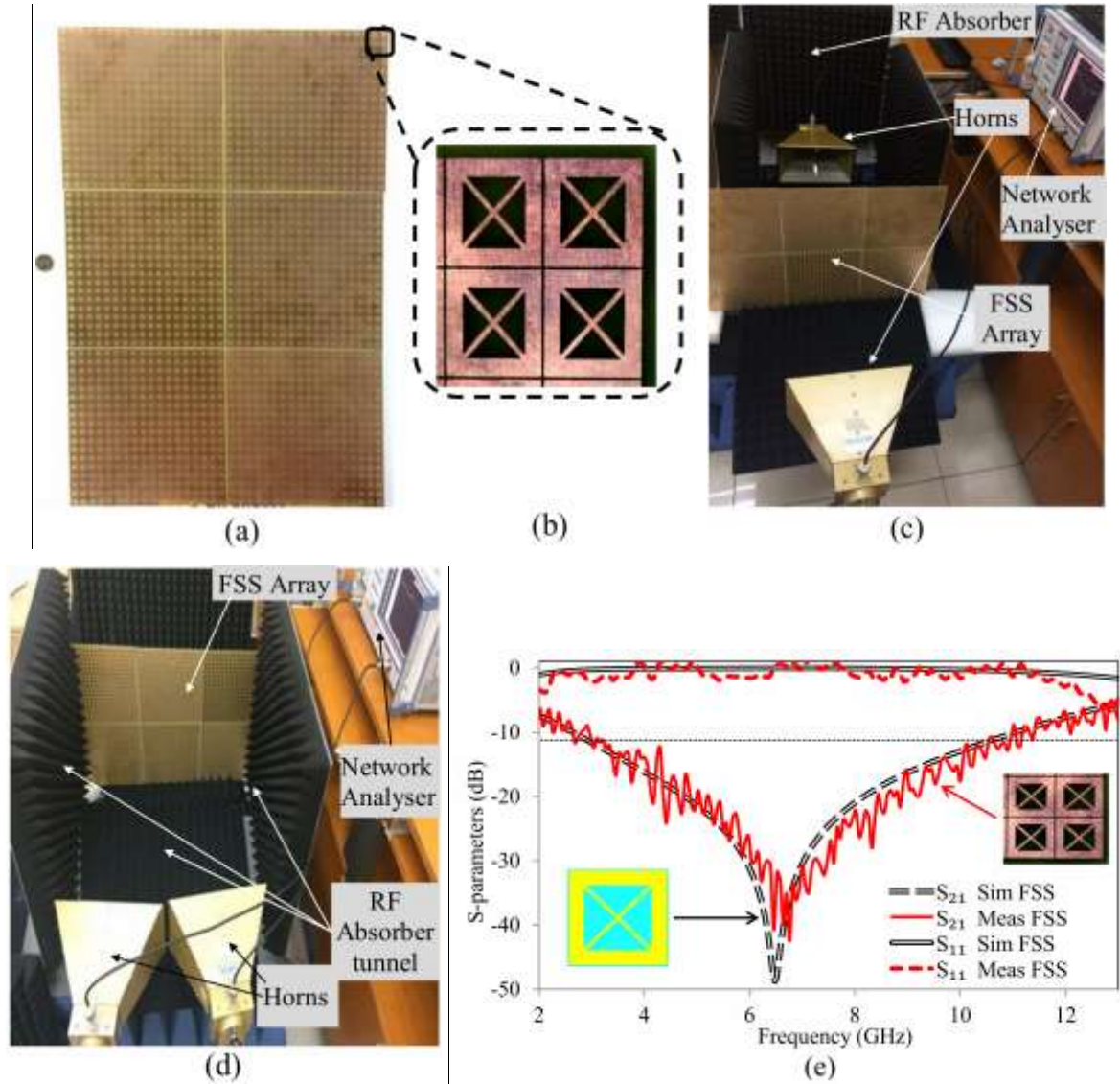


FIGURE 8 (a) Photograph of the FSS array prototype 54×36 elements, (b) zoom-in view of the unit cells, (c) bi-static S_{21} measurement, (d) bi-static S_{11} measurement of FSS array prototype, and (e) simulated and measured S-parameters magnitude of FSS

4.2 | Experimental results of UWB antenna-based uniplanar FSS reflector

The characteristics of fabricated hexagonal monopole antenna were determined and validated with the simulation outcomes for both Antenna #1 without FSS and Antenna #2

with FSS reflector. Figures 9a,b portray the images of Antennas #1 and #2 with 3×3 FSS array prototypes, respectively. To hold the design structure during measurement, the substrates of the antenna and the FSS array were increased by 10 mm at both left and right sides. This aided in combining the antenna with FSS via spacers. The air spacing distance, D_z , was maintained by using Teflon spacers between the monopole antenna and the FSS array. The size of the proposed design (Antenna #2) was only $30 \times 31.9 \times 21.6 \text{ mm}^3$.

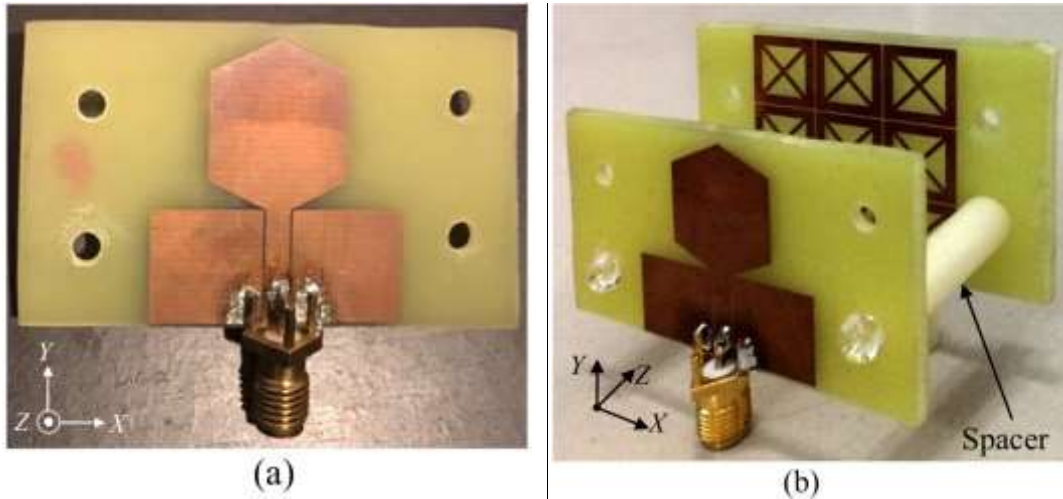


FIGURE 9 Prototypes of (a) Antenna #1, and (b) Antenna #2

The S_{11} magnitudes of Antennas #1 and #2 were measured with B&S ZVB14 Vector Network Analyzer. The comparison between the simulated and the measured S_{11} magnitudes is presented in Figure 10 to propose hexagonal Antennas #1 and #2. As a result, good agreement was achieved between the simulated and the measured S_{11} for both antennas. Antenna #1 displayed the operation bandwidth ranging from 3.4 until 10.7 GHz, while the bandwidth of Antenna #2 reduced slightly within the range from 3.8 until 10.6 GHz. The antenna bandwidth decreased at lower and higher edges due to the phase matching. The S_{11} magnitude of Antenna #2 enhanced at 6 GHz due to the phase matching of both the direct and the reflected radiation. This slight variation between the simulated and measured outcomes had been due to fabrication inaccuracies, Teflon spacers, and SMA connector losses (matching range between DC and 12 GHz).

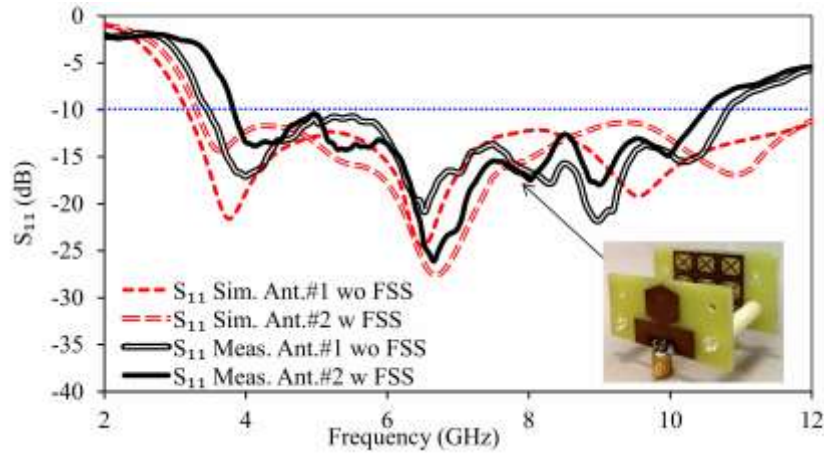


FIGURE 10 S_{11} measurement and simulation of Antenna #1 and Antenna #2

Next, the performances of Antennas #1 and #2 were compared to verify the improvement brought by the proposed FSS reflector. Figure 11 illustrates the simulation and measurement peak gains of Antennas #1 and #2. The measured gain for Antenna #1 changed from 1 to 6 dBi at measurement spectrum. Likewise, Antenna #2 resulted in high measured gain values from 2 to 8 dBi. The simulation gain of Antenna #2 that improved by 3.8 dBi; higher than that for Antenna #1 over UWB spectrum. Hence, the measured gain of Antenna #2 enhanced by about 3.5 dBi by using only 3×3 FSS array at 21.6 mm spacing. As such, higher gain of Antenna #2 can be obtained by increasing the number of the unit cells (such as 5×5 or 7×7) for the FSS array (including increment in design size). Reducing the spacing distance, D_z , also increased antenna gain, but decreased the bandwidth. Thus, embedding the proposed FSS array behind the monopole antenna can substantially enhance the gain at the broad bandwidth.

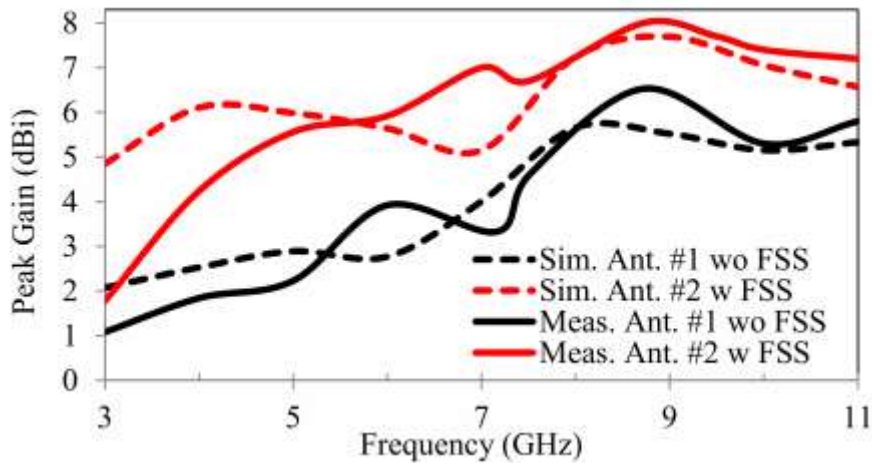


FIGURE 11 The measurement and simulation gain results of Antenna #1 and Antenna #2

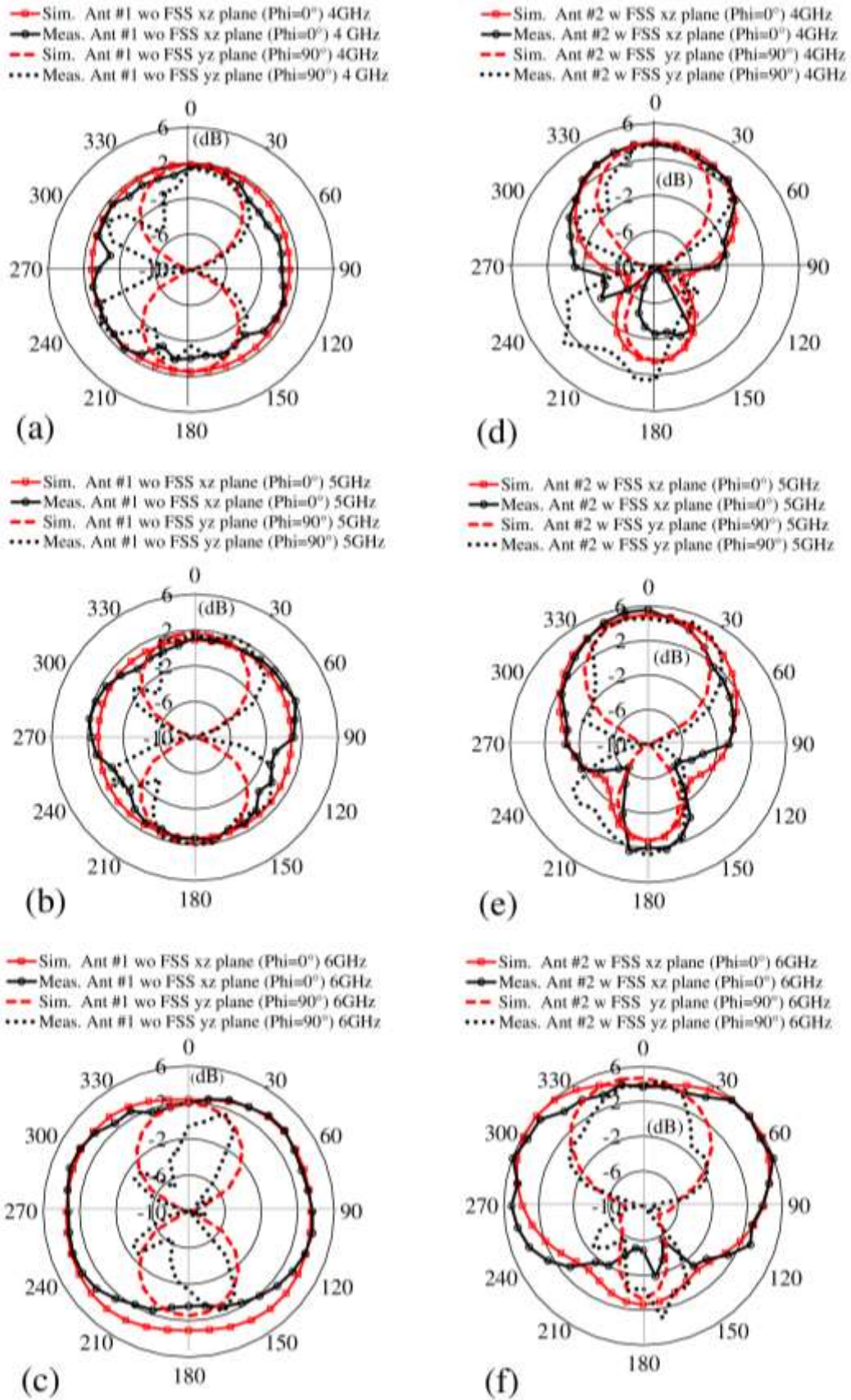


FIGURE 12 The simulation in comparison to measurements radiation patterns of Antenna #1 in (a, b, and c) and Antenna #2 in (d, e, and f) at 4, 5, and 6 GHz

After that, the measured and simulated radiation patterns of Antennas #1 and #2 were compared, as shown in Figure 12. The outcomes are presented in both E-plane (yz plane) and H-plane (xz plane) at 4, 5, and 6 GHz frequencies. Typically, the hexagonal patch of Antenna #1 generated the omnidirectional radiation pattern of H-plane, whereas the UDRs of H- and E-planes were attained at the tested frequencies of Antenna #2 with FSS array. The 3 dB angular beam width H-plane of Antenna #2 was directed to Theta angles of 0° , 0° , and 30° at 4, 5, and 6 GHz, respectively. The radiation pattern exhibited good agreement between the simulation and measurement outcomes. A further narrow beam width was noted by increasing the FSS array elements, which also increased the design size. In precise, the proposed low-cost single-layer compact FSS successfully reflected the monopole antenna radiation patterns over the broad bandwidth.

5 | MWI MODEL AND RESULTS

To verify the ability of the suggested antenna for MWI applications, several metallic objects were hidden inside a simulated handbag model by using the CST Microwave Studio as a case study. In the MWI approach, the scattering data must be recorded at multiple points along the test area (scanning plane) to attain high resolution. The simulated handbag model with scanning scheme is shown in Figure 13a by using the proposed antenna. The bag was made of a textile material with dielectric constant approximately $\epsilon_r = 1.85$ [27] and a 3D size of $110 \times 140 \times 70 \text{ mm}^3$. Three metallic strips were formed in rectangular shape and size $10 \times 20 \times 10 \text{ mm}^3$. After that, the strips were set vertically and horizontally at various locations in the modeled handbag.

In this study, the monostatic approach was applied by using a 2D linear scanning method. The proposed antenna was pointed at a distance Rd of 110 mm from the tested model for short distance detection with complete operating bandwidth. Figure 13b shows that the transmuted Gaussian pulse signal was generated as a default input signal of the software. The design was simulated with a carrier frequency at bandwidth ranging between 3 and 14 GHz. During the linear scanning, the transmitted signals were reflected from the bag model and recorded based on the monostatic approach at a particular time. The outputs that reflected signals within the time domain were recorded from the simulation at 121 points along with the area of $110 \times 110 \text{ mm}^2$ of the model. This scheme portrayed a step-shift (Δx and Δy) of 10 mm between every two adjacent scanned points.

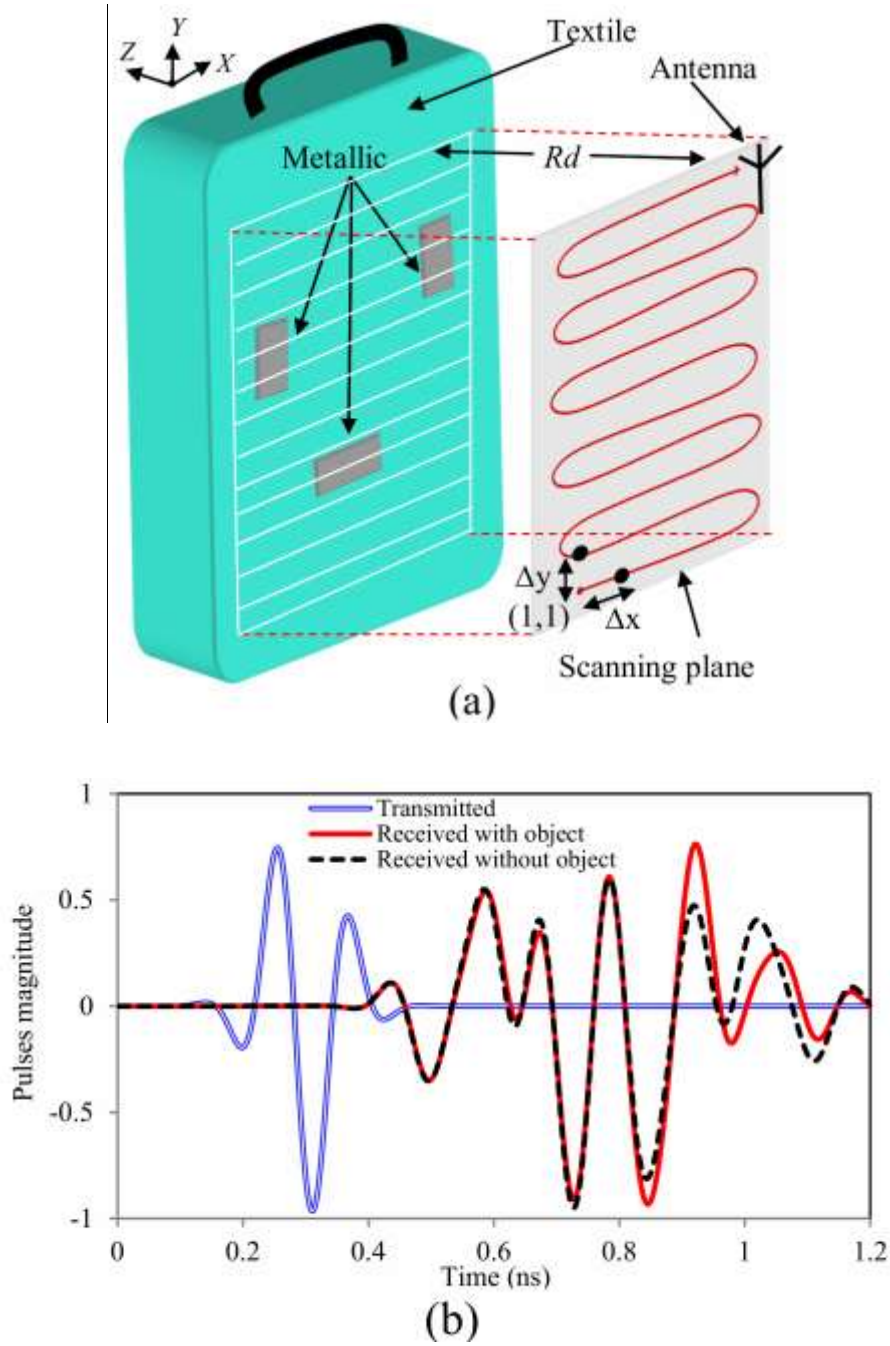
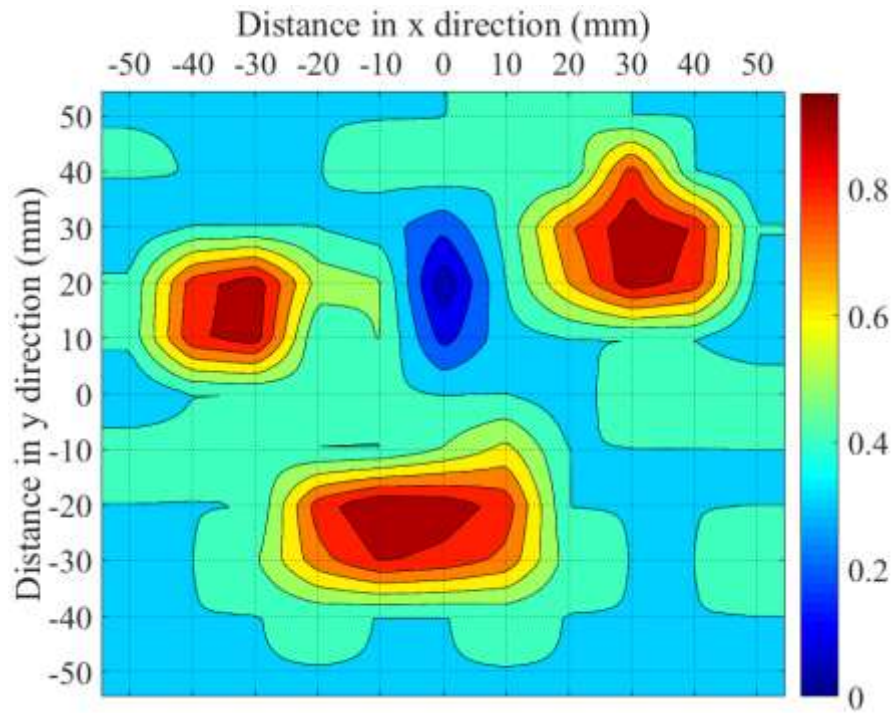


FIGURE 13 (a) 3D view of the handbag model and scanning scheme, (b) normalized transmitted and received signals

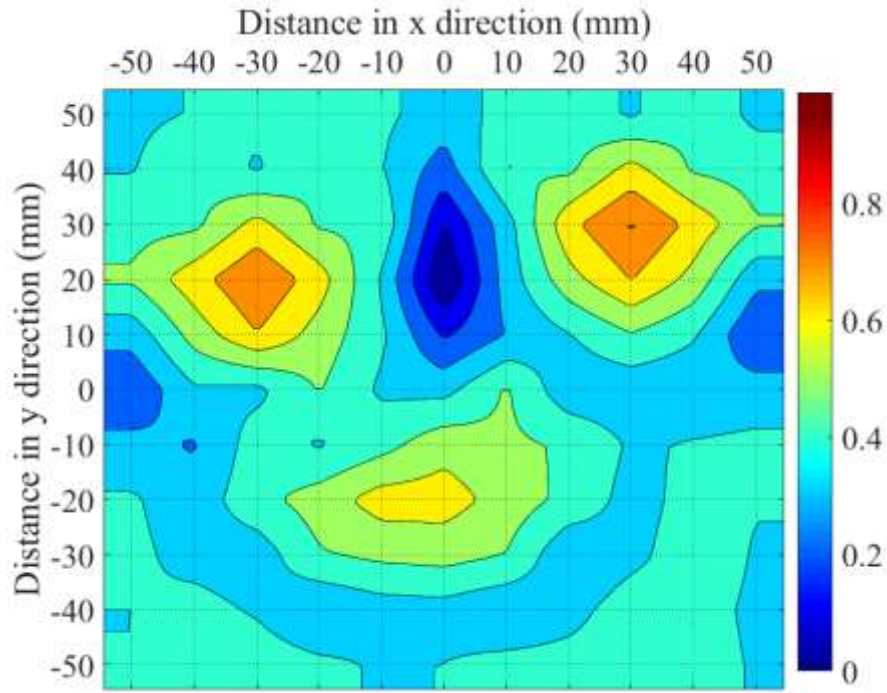
The normalized received signals within the time domain were analyzed by using MATLAB. The received signals of 121 scanned iterations were recorded into two matrices. In the first matrix, the y-axis presented the scanned iterations at varied locations, while the x-axis received the time (nanosecond [ns]). In the second matrix, the x-axis represented normalized received signal magnitude with similar indices of the time matrix. The magnitudes of the received signals fluctuated at 0.92 ns, as displayed in Figure 13b. The

recorded time represented the distance from the antenna using propagation rates in various media. The data were mapped to the image matrix for further imaging process.

Next, the data were compared to determine the time (0.92 ns) that produced the highest varied peaks. The maximum different packs were recorded in the new image matrix of the 121 scanned locations. A 2D image was plotted in (x, y) coordinates. For image evaluation, the proposed imaging process was implemented twice of Antenna #1 without FSS and Antenna #2 with FSS. Figure 14 illustrates the scanned images of the simulated model within the time domain. The 2D image in Figure 14a clearly shows that the metallic objects were visible at the exact spots based on enhanced Antenna #2. Nonetheless, Antenna #1 without FSS gave a low resolution image in Figure 14b due to low antenna gain. The dark red area within the time domain output presented higher reflection magnitudes. In precise, the proposed design is suitable for MWI applications.



(a)



(b)

FIGURE 14 2D images of the scanned model by using Antenna #2 **with FSS in)a (and Antenna #1 without FSS in(b)**

The image presents three objects (red) with high resolution, in comparison to the background (blue). High accuracy of ± 5 mm recorded the location of the objects due to antenna size and scanning step-shift (10 mm). However, more processes were required to display the exact shape and features of the objects. The image also showed the size of the objects; $15 \times 15 \text{ mm}^2$, $20 \times 20 \text{ mm}^2$, and $15 \times 25 \text{ mm}^2$. The proposed scheme obtained a scanning image by using low-complexity signal-processing and low-cost microwave detection approach by considering image resolution. The monostatic approach propagated the signals in the UWB bandwidth. The proposed antenna detected the scattered signals, in which three objects were vividly detected, as displayed in Figure 14a.

Practically, the monostatic systems perform the same antenna for both transmitting and receiving signals, respectively. The antenna in the UWB detection system first transmits a pulse within a short time period, and then the system switches the mode and starts receiving scattered signal for another time period. The received signal is reflected from the echoes of the transmitted energy that are scattered from the target. The received signal represents the RF energy of the scattered signal due to the target size and material, while the travelling time through the media represents the distance, Rd , between the target and the antenna. This

system is usually much cheaper than the bi- static system because it requires fewer antennas and RF cables, but it is utilized for short distance detection applications.

The design of Antenna #2 was $30 \times 31.9 \times 21.6 \text{ mm}^3$ size. In this study, both UWB antenna and FSS unit cell were miniaturized. FSS size, bandwidth, layers, and reflection phase in the literature were compared with the proposed FSS, as tabulated in Table 2. The proposed system was smaller in size, generated high gain, gave UDRs, and cost-effective for manufacturing. Therefore, the proposed design is indeed suitable for MWI applications.

TABLE 2. Parametric comparison of the literature that used FR4 substrate

References	Unit cell size	Stop bandwidth (GHz) $S_{21} < -10\text{dB}$	Reflection phase (S_{11})	Number of FSSs planes
[16]	$0.22\lambda \times 0.22\lambda$	4–12	Nonlinear	Two
[18]	$0.188\lambda \times 0.188\lambda$	3.9–11.1	Linear	Two
[6]	$0.158\lambda \times 0.158\lambda$	3.4–12.9	Linear	Two
[20]	$0.153\lambda \times 0.153\lambda$	4.6–16	–	Two
[14] and [15]	$0.146\lambda \times 0.146\lambda$	4–7	Nonlinear	Two
[19]	$0.14\lambda \times 0.14\lambda$	3–12	Linear	Two
[7]	$0.135\lambda \times 0.135\lambda$	2.7–13.2	–	Four
[17]	$0.108\lambda \times 0.108\lambda$	3–15	Nonlinear	Two
Proposed	$0.095\lambda \times 0.095\lambda$	2.6–11.1	Linear	One

6 | CONCLUSION

In this article, the gain enhancement of UWB monopole antenna CPW-fed based on compact uniplanar FSS array for MWI application was explored. For that purpose, this study built a single-layer small-size FSS unit cell based on copper cross-dipole and square-ring on FR4 substrate as UWB reflector. The miniaturized FSS unit cell size of $0.095\lambda \times 0.095\lambda$ experimentally observed low transition coefficient of -49 dB, broad bandwidth of 2.6 to 11.1 GHz, and linear phase reflection, which had been in line with the outcomes of both the simulated equivalent circuit and the measured 54×36 FSS array prototype. Next, the fabricated hexagonal patch monopole UWB antenna CPW-fed with FSS array realized the broad bandwidth from 3.8 to 10.6 GHz. At an optimum air-gap of 21.6 mm, the gain of UWB antenna was enhanced by about 3.5 dBi with the application of 3×3 FSS array. In the experiment, the characteristics of the proposed antenna were evaluated in two cases; with and without FSS. The UWB monopole antenna with FSS generated UDRs patterns. A good

agreement was observed between the measured and the simulated characteristics. Subsequently, the proposed antennas with and without FSS array were used to scan a new simulated handbag model using CST, which detected metallic objects based on the MWI baggage scanner system. The antenna with FSS displayed image with higher resolution, when compared to that exhibited by antenna without FSS via MATLAB. The developed low-complexity imaging system gave high accuracy of ± 5 mm location for the three small (1×2 cm²) objects due to the high performance of the developed antenna for practical verification. Forthcoming, experimental preparation to scan a conventional handbag is considered for practical imaging evaluation. In summary, miniaturizing the size and maximizing the gain of the proposed design gave excellent resolution of the MWI system. Although the UWB monopole antenna with miniaturized FSS was small in size, it successfully offered higher gain, broader bandwidth, better UDRs, easy-to-setup, and cost-effective, hence a potential candidate for early detection of concealed objects in passenger luggage security application.

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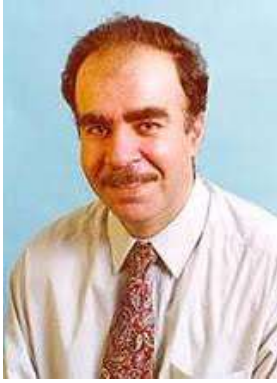
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